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An exact formula is obtained for the equilibrium temperature of a surface in a stream of hot gas. The heat-transfer coefficient is supposed known.

In the study of aerohydrodynamic heating it is frequently necessary to know the equilibrium temperature of a surface, T_{eq} , determined by the heat balance between convective heat flow and radiative transfer:

$$\alpha \left(T_e - T_{eg}\right) = \varepsilon \sigma T_{eg}^4 \,. \tag{1}$$

Up to the present time this equation has been solved graphically, by the method of successive approximations, or by approximate formulas [1]. We present the derivation of an exact analytic formula for the equilibrium temperature of a surface when the heat-transfer coefficient α is known.

We transform Eq. (1) to the form

$$T_{eq}^{4} + \frac{\alpha T_{eq}}{\varepsilon \sigma} - \frac{\alpha T_{e}}{\varepsilon \sigma} = 0.$$
 (1')

The roots of this equation coincide with the roots of two quadratic equations [2]

$$T_{eq}^{2} + A \frac{T_{eq}}{2} + y - \frac{\frac{\omega}{\epsilon\sigma}}{A} = 0, \qquad (2)$$

where $A = \pm \sqrt{8y}$ and y is the real root of the cubic equation

$$8y^{3}+8 \frac{\alpha T_{e}}{\varepsilon \sigma} y - \left(\frac{\alpha}{\varepsilon \sigma}\right)^{2} = 0, \qquad (3)$$

which reduces to

$$y^3 + 3py - 2q = 0. \tag{3'}$$

Since the discriminant $D = q^2 + p^3 > 0$, Equation (3') has one real root which can be found from the Cardan solution: y = u + v, where

$$u = \sqrt[3]{-q + \sqrt{q^2 + p^3}}, v = \sqrt[3]{-q - \sqrt{q^2 + p^3}}.$$

Consequently

$$y = \left[\frac{\alpha^2}{16 \,\varepsilon^2 \sigma^2} + \sqrt{\left(\frac{\alpha^2}{16 \,\varepsilon^2 \sigma^2}\right)^2 + \left(\frac{\alpha T_e}{3 \,\varepsilon \sigma}\right)^3}\right]^{1/3} + \left[\frac{\alpha^2}{16 \,\varepsilon^2 \sigma^2} - \sqrt{\left(\frac{\alpha^2}{16 \,\varepsilon^2 \sigma^2}\right)^2 + \left(\frac{\alpha T_e}{3 \,\varepsilon \sigma}\right)^3}\right]^{1/3}.$$
 (4)

From (2) the equilibrium temperature is

$$T_{\rm eq} = -\frac{A}{4} \pm \sqrt{\frac{A^2}{16} - \left(y - \frac{\alpha}{A\epsilon\sigma}\right)}.$$
 (5)

For $A = -\sqrt{8y}$ we obtain the two complex conjugate roots

$$T_{\rm eq} = \sqrt{\frac{y}{2}} \pm \sqrt{\frac{y}{2}} - \left(y + \frac{\alpha}{\varepsilon\sigma\sqrt{8y}}\right) = \sqrt{\frac{y}{2}} \pm \sqrt{-\frac{y}{2} - \frac{\alpha}{\varepsilon\sigma\sqrt{8y}}}.$$
 (6)

These roots do not correspond to the required real physical solution.

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For positive $A = \sqrt{8y}$

$$T_{eq} = -\sqrt{\frac{y}{2}} \pm \sqrt{-\frac{y}{2} + \frac{\alpha}{\varepsilon\sigma\sqrt{8y}}}$$
 (7)

Since a positive solution is required and y, α , ε , and σ are positive at the equilibrium temperature, there remains the single real positive root

$$T_{\rm eq} = -\sqrt{\frac{y}{2}} + \sqrt{-\frac{y}{2} + \frac{\alpha}{\varepsilon\sigma\sqrt{8y}}}$$
 (8)

Similarly an analytic formula can be obtained for the steady-state temperature of a wall heated by a stream of hot gas on the outside, and cooled from the inside. Thus, for example, for the steady removal of heat through a wall with a heat-transfer coefficient α_{in} , the heat-balance equation has the form:

$$\alpha (T_e - T_{out}) = \varepsilon \sigma T_{out}^4 + \alpha_{in} (T_{out} - T_{in}), \qquad (9)$$

and

$$\alpha_{\rm in} = \frac{\lambda}{\delta} , \qquad (10)$$

....

$$T_{\text{out}} = -\sqrt{\frac{y_1}{2}} + \sqrt{-\frac{y_1}{2} + \frac{\alpha + \alpha_{\text{in}}}{\varepsilon \sigma_V \ 8y_1}}.$$
(11)

where

$$y_{1} = \left[\frac{(\alpha + \alpha_{\mathrm{in}})^{2}}{16 \ \varepsilon^{2} \sigma^{2}} + \sqrt{\left[\frac{(\alpha + \alpha_{\mathrm{in}})^{2}}{16 \ \varepsilon^{2} \sigma^{2}}\right]^{2} + \left(\frac{\alpha T_{e} + \alpha_{\mathrm{in}} T_{\mathrm{in}}}{3 \ \varepsilon \sigma}\right)^{3}}\right]^{1/3} + \left[\frac{(\alpha + \alpha_{\mathrm{in}})^{2}}{16 \ \varepsilon^{2} \sigma^{2}} - \sqrt{\left[\frac{(\alpha + \alpha_{\mathrm{in}})^{2}}{16 \ \varepsilon^{2} \sigma^{2}}\right]^{2} + \left(\frac{\alpha T_{e} + \alpha_{\mathrm{in}} T_{\mathrm{in}}}{3 \ \varepsilon \sigma}\right)^{3}}\right]^{1/3}}.$$
(12)

NOTATION

Tin is the temperature of the inside surface;

T_e is the recovery temperature;

Tout is the temperature of the outside surface;

T_{eq} is the equilibrium temperature;

 α is the coefficient for heat transfer from the hot gas to the surface;

 α_{in} is the coefficient for heat transfer through the wall;

 δ is the wall thickness;

 ϵ is the emissivity;

 λ is the thermal conductivity;

 σ is the Stefan–Boltzmann constant.

LITERATURE CITED

1 N. F. Krasnov, Aerodynamics of Bodies of Revolution, Elsevier, New York (1970).

2. V. I. Smirnov, A Course in Higher Mathematics [in Russian], Vol. 1, GIFML, Moscow (1961).